

(A) 6:30 PM
(B) 5:00 PM
(C) 6:00 PM
(D) 5:30 PM

Ans. B

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Sol.	Given : Three bells P, Q and R rings periodically in a school.					
	P rings in every 20 minutes, Q rings in every 30 minutes and R rings in every 50 minutes.					
	Bells, P, Q and R will ring after the respective Least Common Multiple of ringing time intervals of					
	Least Common Multiple of 20 min 30 min and 50 min is 300 min					
	Where 300 minutes is equals to 5 hours					
	As, all the three bells ranges at 12:00 PM then after 12 PM, the three bells ring together again, after 5 hours at 5 PM.					
	Hence, the correct option is (B).					
Quest	ion 4					
	Given below are two statements and four conclusions drawn based on the statements.					
	Statement 1 : Some bottles are cups.					
	Statement 2 : All cups are knives.					
	Conclusion I : Some bottles are knives.					
	Conclusion II : Some knives are cups.					
	Conclusion III : All cups are bottles.					
	Conclusion IV : All knives are cups.					
	Which one of the following options can be logically inferred?					
	(A) Only conclusion II and conclusion III are correct					
	(B) Only conclusion II and conclusion IV are correct					
	(C) Only conclusion III and conclusion IV are correct					
	(D) Only conclusion I and conclusion II are correct					
Ans.	D					
Sol.	Given : Statement I : Some bottles are cups					
	Statement I : All cups are knives					
	Below figure shows the venn diagram according to given statements,					
	Bottles Cup					
	<b>Conclusion I :</b> Some bottles are knives, is correct as we can see in the figure some part of the bottle is intersect with knives.					
	<b>Conclusion II :</b> Some knives are cups, is correct as we can see in the figure all part of the cup is intersect with knives					
	<b>Conclusion III</b> : All cups are bottles, is not correct as we can see in the figure some part of the cup is					
	intersect with bottle and we have no definite information about remaining part of cup.					
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**Conclusion IV :** All knives are cups, is not correct as we can see in the figure some part of the knives is intersect with cup and we have no definite information about remaining part of knives. Hence, the correct option is (D).

#### **Question 5**

The figure below shows the front and rear view of a disc, which is shaded with identical patterns. The disc is flipped once with respect to any one of the fixed axes 1-1, 2-2 or 3-3 chosen uniformly at random. What is the probability that the disc DOES NOT retain the same front and rear views after the flipping operation?



#### Ans. C

Sol.

(A) 1

(C)  $\frac{2}{3}$ 

If we rotate the disc along 1-1 axis,

We get front as rear and rear as front

That means this is not our favorable outcome.

If we rotated the disc along 2-2 axis,

We do not get front as rear and rear as front.

That means disc does not retain the same and this is our favorable outcome.

If we rotated the disc along 3-3 axis,

We do not get front as rear and rear as front.

That means disc does not retain the same and this is also our favorable outcome.

After the flipping operation the probability that the disc does not retain the same front and rear view is

$$P(E) = \frac{\text{Favorable outcomes}}{\text{Total outcomes}} = \frac{2}{3}$$

Hence, the correct option is (C).

## Q.6 to Q.10 Carry TWO Marks Each

#### **Question 6**

Altruism is the human concern for the wellbeing of others. Altruism has been shown to be motivated more by social bonding, familiarity and identification of belongingness to a group. The notion that altruism may be attributed to empathy or guilt has now been rejected.

Which one of the following is the CORRECT logical inference based on the information in the above passage?

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- (A) Humans engage in altruism due to guilt but not empathy.
- (B) Humans engage in altruism due to group identification but not empathy.
- (C) Human engage in altruism due to empathy but not guilt.
- (D) Human engage in altruism due to empathy but not familiarity.

### Ans. B

**Sol.** Option (A), can not be inferred as here guilty and empathy are used in opposite tone but in passage they are used in similar tone.

Option (B), can be inferred as it is clearly mentioned the term 'due to group identification but not empathy'.

Option (C), can not be inferred as in this option again empathy and guilty are used in different tone.

Option (D), can not be inferred as in this option familiarity is used in negative tone and in passage it is given in positive tone.

Hence, the correct option is (B).

## **Question 7**

There are two identical dice with a single letter on each of the faces. The following six letters : Q, R, S, T, U and V, one on each of the faces. Any of the six outcomes are equally likely.

The two dice are thrown once independently at random.

What is the probability that the outcomes on the dice were composed only of any combination of the following possible outcomes : Q, U and V?

(A) 
$$\frac{1}{6}$$
 (B)  $\frac{3}{4}$   
(C)  $\frac{5}{36}$  (D)  $\frac{1}{4}$ 

Ans. D

**Sol.** Given : Two identical dice with a single letter on each of the faces.

The following six letters : Q, R, S, T, U and V one on each of the faces.

Any of the six outcomes are equally likely.

P(Event) = P(getting outcomes from dice one) . P(getting outcomes from dice two) For favorable outcome we need any one of them Q, U, V

 $P(E) = \frac{\text{Favorable outcomes}}{\text{Total outcomes}}$   $P(E) = \frac{3}{6} \times \frac{3}{6} = \frac{1}{4}$ 

Hence, the correct option is (D).

## **Question 8**

The price of an item is 10% cheaper in an online store S compared to the price at another online store M. Store S charges  $\overline{\mathbf{x}}$  150 for delivery. There are no delivery charges for orders from the store M. A person bought the item from the store S and saved  $\overline{\mathbf{x}}$  100.

What is the price of the item at the online store S (in  $\mathbb{Z}$ ) if there are no other charges than what is described above?

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Ans.	(A) (C) D	1500 1750			(B) (D)	2500 2250	c.		
<b>301</b> .	Given : The price of an item is 10% cheaper in an online store S compared to the price at another online store M. Delivery charges of an item at the online store S and M is $\Xi 150$ and 0 means timely								
	Delivery charges of an item at the online store S and M is $\gtrless 150$ and 0 respectively.							ere M	
	Cost of an item from the online store S is $< 100$ less than the item from online store M.								
	Let, the price of an item at the online store M is $\langle x \rangle$								
	I nen So	price of	an item at the $r = (0.9r + 1)$	50) - 100	s(x -	(0.1x) = 0	0.9 <i>x</i>		
	50,		0.1x - 150 =	100					
			0.1x = 250						
			<i>x</i> = 250						
	The p	price of t	he item at the	online store S (i	in ₹) v	vithout a	ny delivery ch	narges is	,
			$0.9x = 0.9 \times$	250 <mark>= 22</mark> 50					
	Henc	e, the co	rrect option is	(D).					
quoor	<ul> <li>The letters P, Q, R, S, T and U are to be placed one per vertex on a regular convex hexagon, but not necessarily in the same order.</li> <li>Consider the following statements :</li> <li>The line segment joining R and S is longer than the line segment joining P and Q.</li> <li>The line segment joining R and S is perpendicular to the line segment joining P and Q.</li> </ul>								
	• The line segment joining R and U is parallel to the line segment joining T and Q. Based on the above statements, which one of the following options is CORRECT?								
	(A)	The line	segment join	ing T and Q is p	aralle	l to the l	ine joining P a	and U.	
	(B)	The line	segment join	ing Q and S is p	erpen	licular t	o the line segn	nent join	ing R and P.
	(C)	The line	segment join	ing R and T is p	aralle	to the l	ine segment jo	oining Q	and S.
Ans.	(D) C	The fine	segment join	ing R and P is p	erpend	incular u	o the line segn	nent join	ing U and Q.
Sol.	Give	n:							
	The l	etters P,	Q, R, S, T and	l U are to be pla	aced or	ne per ve	ertex on regula	ar conve	x hexagon.
	Given conditions are as follows, The line segment joining R and S is longer then the line segment joining P and Q. RS > PQ								
							Q.		
The line segment joining R and S is perpendicular to the line segment joining P and Q. $RS \perp PQ$									
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## **Technical Section**

## Q.11 to Q.35 Carry ONE Mark Each

#### **Question 11**

**Control System** 

The transfer function of a real system, H(s), is given as :

$$H(s) = \frac{As+B}{s^2+Cs+D}$$

where A, B, C and D are positive constants. This system cannot operate as

(A)	band pass filter	( <b>B</b> )	low pass filter
(C)	an integrator	(D)	high pass filter

#### Ans. C or D

#### **Sol.** Given :

Transfer function of a real system H(s) is given by,

 $H(s) = \frac{As+B}{s^2+Cs+D}$ 

Put  $s = j\omega$  in equation (i),

$$H(j\omega) = \frac{A(j\omega) + B}{(j\omega)^2 + j\omega C + D}$$

Magnitude, 
$$|H(\omega)| = \frac{\sqrt{(A\omega)^2 + B^2}}{\sqrt{(D-\omega)^2 + (\omega C)^2}}$$
...(ii)

**Case 1 :** At low frequency ( $\omega = 0$ ), equation (ii) can be approximated as,

$$\left|H(\omega=0)\right| = \frac{B}{D}$$

It means, low frequency passed by given real system H(s).

At high frequency ( $\omega = \infty$ ), equation (ii) can be approximated as,

$$|H(\omega = \infty)| = 0$$

It means, high frequency blocked by given real system H(s)

Thus, given real system H(s) work as low pass filter but not high pass filter.

**Case 2 :** Assuming *B* is very less positive valued constant as compare to values of positive constant *A*, *C* and *D* then H(s) can be approximated as,

...(i)

$$H(s) = \frac{As}{s^2 + Cs + D}$$

Put  $s = j\omega$  in above equation,

$$H(j\omega) = \frac{A(j\omega)}{(j\omega)^2 + j\omega C + D}$$

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Magnitude, 
$$|H(\omega)| = \frac{(A\omega)^2}{\sqrt{(D-\omega)^2 + (\omega C)^2}}$$

At low frequency ( $\omega = 0$ ),  $|H(\omega = 0)| = 0$ ; it means block low frequency.

At high frequency  $(\omega = \infty)$ ,  $|H(\omega = \infty)| = 0$ ; it means block high frequency.

Magnitude plot of  $|H(\omega)|$  is,



It is given H(s) pass frequency between low frequency and high frequency.

Thus, real system H(s) can work as band pass filter also.

Hence, the correct options is (C) or (D).

Note : This questions is MCQ type but IIT KGP provide two answers for this question, even the real system H(s) can approximate into integrator as shown below :

Under very high value of frequency  $(\omega \rightarrow \infty)$ , the H(s) can be approximated as,

$$H(s) \approx \frac{As}{s^2} \approx \frac{A}{s}$$

Thus, real system H(s) can work as integrator.

#### **Question 12**

#### **Analog Electronics**

For an ideal MOSFET biased in saturation, the magnitude of the small signal current gain for a common drain amplifier is

**(B)** 1

Sinc<sup>®</sup><sup>o</sup>200



(C) 100

```
Ans. A
```

**Sol.** Given :

- (i) MOSFET is ideal
- (ii) Biased under saturation
- (iii) Ideal common drain amplifier

Thus current gain  $(A_I)$  of ideal common drain amplifier

 $A_{I} = \infty$ 

Hence, the correct option is (A).

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As current flow through capacitor  $C_1$  is constant of value  $\frac{0.1}{R_1}$  A, it shows the linear charging of capacitor

 $C_1$ ,



The voltage across the capacitor  $V_c(t)$  under linear charging is,

$$V_{c}(t) = \frac{1}{C_{1}} \int_{0}^{t} \frac{i_{c}(t)dt}{\int_{0}^{t} \frac{1}{R_{1}} dt} = \frac{0.1}{R_{1}C_{1}} t$$

$$Q_{c}(t) = \frac{1}{C_{1}} \int_{0}^{t} \frac{0.1}{R_{1}} dt = \frac{0.1}{R_{1}C_{1}} t$$

So, graph between  $V_c(t)$  verses t, is a linear line as shown below



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From above graph it is clear that, capacitor charged continuously upto infinite time. Thus from equation (i),

$$V_{out} = -V_c(t) = -\frac{0.1}{R_1 C_1} t$$

The graph of  $V_{out}$  is shown below,



Under steady state  $(t = \infty)$ ,  $V_{out} = -V_c(\infty) = -\infty$ 

Thus, Op-Amp does not allow  $V_{out}$  to be  $-\infty$  so, Op-Amp will saturate to  $-V_{EE}$  so that

$$V_{out} = -V_{EE}$$

Hence, the correct option is (A).

#### Avoid this Mistake :

- Don't make capacitor open circuit under steady-state condition because constant current is flowing through capacitor so it is the case of linear charging of capacitor.
- Many aspirant try to think that under steady state capacitor is open circuit and Op-Amp behave as comparator and  $V^+ < V^-$  in given circuit due to this, you will get answer  $V_{out} = -V_{EE}$  but conceptually it is wrong because it is the case of linear charging of capacitor.



#### **Question 17**

**Control Systems** 

The Bode magnitude plot of a first order stable system is constant with frequency. The asymptotic value of the high frequency phase, for the system, is  $-180^{\circ}$ . This system has





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(A) one LHP pole and one RHP zero at the same frequency.

- **(B)** one LHP pole and one LHP zero at the same frequency.
- two LHP poles and one RHP zero. (C)
- (D) two RHP poles and one LHP zero.

#### A Ans.

Given bode magnitude and phase plot of a first order stable system is shown below. Sol.



Flat constant magnitude response for all frequency of system shows that it is an all pass system. In all pass system, poles and zeros are symmetrical about  $j\omega$  axis.

shows  $\phi = -180^{\circ}$ 

The possible transfer functions all pass system are

$$T_{1}(s) = \frac{s-1}{s+1}$$

$$T_{2}(s) = \frac{1-s}{1+s}$$
From the phase plot as  $\omega \rightarrow \infty$  shows  $\phi = -180^{\circ}$ 
For  $T_{1}(s)$  :
$$T_{1}(s) = \frac{s-1}{s+1}$$
Put  $s = j\omega$ 

$$T_{1}(j\omega) = \frac{j\omega-1}{j\omega+1}$$
Since
$$\angle T_{1}(j\omega) = 180^{\circ} - \tan^{-1}\omega - \tan^{-1}\omega = 180^{\circ} - 2\tan^{-1}\omega$$
At  $\omega = \infty$ ,
$$\angle T_{1}(j\infty) = 180^{\circ} - 2\tan^{-1}\infty$$

$$\angle T_{1}(j\infty) = 0^{\circ}$$

For  $T_2(s)$ :

$$T_2(s) = \frac{1-s}{1+s}$$

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Put  $s = j\omega$ ,

$$T_{2}(j\omega) = \frac{1-j\omega}{1+j\omega}$$
  

$$\angle T_{2}(j\omega) = -\tan^{-1}\omega - \tan^{-1}\omega = -2\tan^{-1}\omega$$
  
At  $\omega = \infty$ ,  

$$\angle T_{2}(j\omega) = -2\tan^{-1}\infty$$
  

$$\angle T_{2}(j\omega) = -180^{0}$$

Hence, the transfer function of given all pass filter.

$$T(s) = \frac{1-s}{1+s}$$

Hence, the system has one LHP pole and one RHP zero at the same frequency.

Hence, the correct option is (A).

#### **Question 18**

#### Measurement

A balanced Wheatstone bridge *ABCD* has the following arm resistances :  $R_{AB} = 1 \text{ k}\Omega \pm 2.1\%$ ;

 $R_{BC} = 100 \ \Omega \pm 0.5\%$ ;  $R_{CD}$  is an unknown resistance;  $R_{DA} = 300 \ \Omega \pm 0.4\%$ . The value of  $R_{CD}$  and its accuracy is

(A)  $3000 \Omega \pm 90 \Omega$ (B)  $3000 \Omega \pm 3 \Omega$ (C)  $30 \Omega \pm 0.9 \Omega$ (D)  $30 \Omega \pm 3 \Omega$ 

#### Ans. C

#### **Sol.** Given :

Balanced Wheatstone bridge ABCD, has the following arm's resistance are,

 $R_{AB} = 1 \text{ k}\Omega \pm 2.1\%$  $R_{BC} = 100 \ \Omega \pm 0.5\%$  $R_{DA} = 300 \ \Omega \pm 0.4\%$ 

#### Calculate :

The value of  $R_{CD}$  and its accuracy is,



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Now, %RLE error is defined as the formula,  $\% \varepsilon = \frac{\delta R_{CD}}{R_{CD}} \times 100$  $\delta R_{CD}$  = Absolute error  $\delta R_{CD} = \% \epsilon \times R_{CD}$  $\delta R_{CD} = \frac{3}{100} \times 30 = \frac{9}{10} = 0.9 \ \Omega$  $R_{CD} = 30 \ \Omega \pm 0.9 \ \Omega$ Hence, the correct option is (C). **General Key Point** Absolute error : It is defined it is the difference between measured value and true value.  $\delta A = A_m - A_T$ Where,  $\delta A = Absolute error$ ,  $A_m = Measured$  value and  $A_T = True$  value. (ii) %REL is defined, it is the ratio of absolute error to the true value.

**Control Systems** 

$$\% RLE = \% \varepsilon = \frac{\delta A}{A_T} \times 100$$

#### **Question 19**

(i)

The open loop transfer function of a unity gain negative feedback system is given by,

$$G(s) = \frac{K}{s^2 + 4s - 5}$$

The range of K for which the system is stable, is

$$(A) \quad K > 3$$

(B) K < 5

(D) K > 3

ince

Ans. Δ

$$G(s) = \frac{K}{s^2 + 4s - \xi}$$

< 3

The characteristic equation is given by,

$$1 + G(s) = 0$$

$$1 + \frac{K}{s^2 + 4s - 5} = 0$$
  
$$s^2 + 4s - 5 + K = 0$$
  
$$s^2 + 4s + K - 5 = 0$$

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	Routh tabulation : $s^{2}$ 1 $K-5$ $s^{1}$ 4 $s^{0}$ $K-5$ For the system to be stable, all the roots must be in the left half of $s$ – plane, thus all the coefficients in the first column of Routh tabulation must have the same sign. Therefore, the coefficient of first column of the Routh's table should be positive. Therefore for stability K-5>0 K>5 Hence, the correct option is (A).
	For stability of second order system all coefficient of characteristic equation should be positive.
Quest	ion 20 Mathematics
Ans. Sol.	(A) null. (B) symmetric. (C) skew-symmetric. (D) unitary. <b>C</b> <b>Given:</b> $A = [aij]_{3\times3}, aij = (i-j)^3 \forall i \text{ and } j$ $A = \begin{bmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{bmatrix}_{3\times3}$ $A = \begin{bmatrix} (1-1)^3 & (1-2)^3 & (1-3)^3 \\ (2-1)^3 & (2-2)^3 & (2-3)^3 \\ (3-1)^3 & (3-2)^3 & (3-3)^3 \end{bmatrix}_{3\times3}$ $A = \begin{bmatrix} 0 & -1 & -8 \\ 1 & 0 & -1 \\ 8 & 1 & 0 \end{bmatrix}_{3\times3}$ If we take transpose of matrix A. $A^T = \begin{bmatrix} 0 & 1 & 8 \\ -1 & 0 & 1 \\ -8 & -1 & 0 \end{bmatrix}_{3\times3}$

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$$-A^{T} = \begin{bmatrix} 0 & -1 & -8 \\ 1 & 0 & -1 \\ 8 & 1 & 0 \end{bmatrix}_{3\times 3}$$

We can see that,  $A = -A^T$ 

So, matrix *A* is skew symmetric matrix.

Hence, the correct option is (C).

#### **Question 21**

#### **Network Theory**

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HATE A

In the circuit shown below, a three-phase star-connected unbalanced load is connected to a balanced threephase supply of  $100\sqrt{3}$  V with phase sequence *ABC*. The star connected load has  $Z_A = 10\Omega$  and  $Z_B = 20\angle 60^0\Omega$ . The value of  $Z_C$  in  $\Omega$ , for which the voltage difference across the nodes *n* and *n'* is zero, is



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In case of balance system,  $V_n = 0$  V

By varying  $Z_c$  we can make  $V_n' = 0$  V

n and n' are at same potential

Applying KCL at node n'

$$\frac{0 - 100\sqrt{3} \angle 0^{0}}{10} + \frac{0 - 100\sqrt{3} \angle -120^{0}}{20 \angle 60^{0}} + \frac{0 - 100\sqrt{3} \angle 120^{0}}{Z_{c}} = 0$$

$$10\sqrt{3} + 5\sqrt{3} \angle -180^{0} + \frac{100\sqrt{3} \angle 120^{0}}{Z_{c}} = 0$$

$$5\sqrt{3} \angle 0^{0} + \frac{100\sqrt{3} \angle 120^{0}}{Z_{c}} = 0$$

$$5\sqrt{3} \angle 0^{0} = \frac{-100\sqrt{3} \angle 120^{0}}{Z_{c}}$$

$$Z_{c} = \frac{-100\sqrt{3} \angle 120^{0}}{5\sqrt{3} \angle 0^{0}}$$

$$Z_{c} = 20 \angle -60^{\circ}$$

Hence, the correct option is (D).

#### **Question 22**

A charger supplies 100 W at 20 V for charging the battery of a laptop. The power devices, used in the converter inside the charger, operate at a switching frequency of 200 kHz. Which power device is best suited for this purpose?

(A) Thyristor (C) BJT

- (B) MOSFET
- (D) IGBT

#### Ans. B

Sol. For high switching frequency and low voltage operation, the best suitable device is MOSFET.

Hence, the correct option is (B).

#### **Question 23**

A long conducting cylinder having a radius 'b' is placed along the z axis. The current density is  $\mathbf{J} = J_a r^3 \hat{z}$ for the region r < b where r is the distance in the radial direction. The magnetic field intensity (**H**) for the region inside the conductor (i.e. for r < b) is

(A) 
$$\frac{J_a}{3}r^3$$
  
(B)  $\frac{J_a}{4}r^3$   
(C)  $J_ar^3$   
(D)  $\frac{J_a}{5}r^4$ 

Ans.

## **Power Electronics**

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#### **Electromagnetic Field**

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Here, consider only  $\phi$ -direction component of  $\overline{H}$  and  $d\overline{l}$ , because we have to find  $\overline{H}$  inside the conductor region.

From Ampere's circuital law,  $\oint \overline{H} \cdot d\overline{l} = I_{enclosed}$ 

$$\begin{split} \oint H_{\phi} \hat{a}_{\phi} \cdot d\overline{l} &= I_{enclosed} \\ \because \quad d\overline{l} &= rd\phi \hat{a}_{\phi} \\ \oint H_{\phi} \hat{a}_{\phi} \cdot rd\phi \hat{a}_{\phi} &= I_{enclosed} \\ H_{\phi} rd\phi &= I_{enclosed} \\ H_{\phi} r \oint d\phi &= I_{enclosed} \\ H_{\phi} r \times 2\pi = I_{enclosed} \\ 2\pi rH_{\phi} &= I_{enclosed} \\ 1 &= \oint_{S} J \cdot d\overline{S} \\ \end{split}$$
Here,  $\overline{J}$  is in  $\hat{a}_{z}$  direction, so as must be in  $\hat{a}_{z}$  direction. So  $d\overline{s} = rdrd\phi \hat{a}_{z}$ .  
 $I &= \oint_{S} (J_{\phi} r^{3} \hat{a}_{z}) \cdot (rdrd\phi) \hat{a}_{z} \\ I &= J_{0} \int_{0}^{r} r^{4} dr \int_{\phi=0}^{2\pi} d\phi \\ I &= J_{0} \frac{r^{5}}{5} (2\pi)$   $(\because \hat{a}_{z} \cdot \hat{a}_{z} = 1) \\ I &= J_{0} \frac{2\pi}{5} (r^{5})$  ...(ii)

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Compare equation (i) and (ii),

$$H_{\phi}(2\pi r) = J_0 \frac{2\pi}{5} (r^5)$$
$$H_{\phi} = J_0 \left(\frac{r^4}{5}\right)$$

Thus, 
$$\overline{H} = H_{\phi}\hat{a}_{\phi} = J_0 \left(\frac{r^4}{5}\right)\hat{a}_{\phi}$$

Hence, the correct option is (D).

## **Question 24**

The type of single-phase induction motor, expected to have the maximum power factor during steady state running condition, is

- (A) capacitor start
- (C) capacitor start, capacitor run
- (B) split phase (resistance start) (D) shaded pole

#### Ans. С

Sol. Under steady state running condition power factor of capacitor start capacitor run (CSCR) induction motor is high because one capacitor is permanently connected to the circuit, which improves the running power factor.

Hence, the correct option is (C).

## **Question 25**

For the circuit shown below with ideal diodes, the output will be



## Ans.

Given circuit with ideal diodes is shown below, Sol.



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## **Electrical Machine**

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**Analog Electronics** 



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## For Positive half cycle :

 $D_1$  and  $D_2$  will be ON, and replace by short circuit. So circuit becomes as,



Here,

## For Negative half cycle :

 $D_1$  and  $D_2$  will be OFF, and replace by open circuit. So circuit becomes as,



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#### Method 1

Overall Q-factor of series combination of inductor and capacitor is given by,



Hence, the overall Q-factor of series combination of inductor and capacitor is 48.

#### Method 2

Overall Q-factor of series combination of inductor and capacitor is given by,



Hence, the overall Q-factor of series combination of inductor and capacitor is 48.

#### **Question 28**

The network shown below has a resonant frequency of 150 kHz and a bandwidth of 600 Hz. The *Q*-factor of the network is \_\_\_\_\_. (round off to nearest integer)

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#### **Network Theory**





#### Ans. 250 (Range : 250 to 250)

**Sol.** Given : Resonant frequency 
$$f_0 = 150 \text{ kHz}$$

Bandwidth  $\Delta f = 600 \text{ Hz}$ 

Q factor of RLC circuit in terms of resonant frequency and bandwidth is given by,

$$Q = \frac{\text{Resonant frequency}}{\text{Bandwidth}} = \frac{f_0}{\Delta f}$$
$$Q = \frac{150 \times 10^3}{600}$$
$$Q = 250$$

Hence, the value of Q factor of circuit is 250.

#### **Question 29**

The maximum clock frequency in MHz of a 4-stage ripple counter, utilizing flip-flops, with each flip-flop having a propagation delay of 20 ns, is \_\_\_\_\_\_. (round off to one decimal place).

#### Ans. 12.5 (Range : 12.3 to 12.7)

**Sol.** Given :

- (i) 4-stage ripple counter
- (ii) Number of bits n = 4
- (iii) Propagation delay of each flip-flop  $t_{pd} = 20$  nsec
- (iv) Maximum clock frequency of *n*-state ripple counter,

$$f_{CLK} = \frac{1}{nt_{pd}} = \frac{1}{4 \times 20 \times 10^{-9}} = 12.5 \text{ MHz}$$

Hence, the correct answer is 12.5.

#### **Question 30**

If only 5% of the supplied power to a cable reaches the output terminal, the power loss in the cable, in decibels, is \_\_\_\_\_. (round off to nearest integer)

#### Ans. 13 (Range : 13 to 13)

#### **Sol.** Given :

Power reaches at output terminal  $(P_{out}) = 5\%$  of the supplied power  $(P_{in})$ .

Power loss in decibels (dB), in cable =  $10 \log \left(\frac{P_{in}}{P_{out}}\right) = 10 \log P_{in} - 10 \log P_{out}$ 

#### **Digital Electronics**

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**Power System** 

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Power loss in decibels (dB), in cable =  $10 \log \frac{P_{in}}{0.05 P_{in}} = 10 \log 20$ 

Power loss in decibels (dB), in cable =13.01 dB  $\approx$ 13 dB

Hence, the power loss in the cable, in decibels is 13 dB.

#### **Question 31**

#### **Network Theory**

In the circuit shown below, the switch *S* is closed at t = 0. The magnitude of the steady state voltage, in volts, across the  $6\Omega$  resistor is \_\_\_\_\_. (round off to two decimal places).



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GATE A

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Hence, the magnitude of steady state voltage across  $6\Omega$  resistor is 5 V.

#### **Question 32**

#### **Power Electronics**

A single-phase full-bridge diode rectifier feeds a resistive load of 50  $\Omega$  from a 200 V, 50 Hz single phase AC supply. If the diodes are ideal, then the active power, in watts, drawn by the load is \_\_\_\_\_. (round off to nearest integer)

#### Ans. 800 (Range : 795 to 805)

#### Sol. Given :

- (i)  $1-\phi$  full bridge rectifier.
- (ii) Resistive load,  $R = 50 \Omega$
- (iii) Supply voltage,  $V_{s(rms)} = 200 \text{ V}$
- (iv) Frequency, f = 50 Hz

Peak voltage,  $V_m = V_{s(rms)} \times \sqrt{2} = 200\sqrt{2}$  Volts

The active power drawn by the load in watts.



We know, average output power for the resistive load is given by,

$$P_{0(avg)} = \frac{V_{0(rms)}^2}{R}$$

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For 1- $\phi$  full bridge diode rectifier, in case of resistive load,

$$V_{0(rms)} = V_{s(rms)} = 200 \text{ V}$$
  
 $P_0(\text{avg}) = \frac{200^2}{50} = 800 \text{ W}$ 

Hence, the correct answer is 800 W.

#### **Question 33**

#### **Power Electronics**

steps to success.

The voltage at the input of an AC-DC rectifier is given by  $v(t) = 230\sqrt{2} \sin \omega t$  where  $\omega = 2\pi \times 50$  rad/sec. The input current drawn by the rectifier is given by

$$i(t) = 10\sin\left(\omega t - \frac{\pi}{3}\right) + 4\sin\left(3\omega t - \frac{\pi}{6}\right) + 3\sin\left(5\omega t - \frac{\pi}{3}\right).$$

The input power factor, (rounded off to two decimal places), is, \_\_\_\_\_ lag.

## Ans. 0.4473 (Range : 0.43 to 0.47)

#### **Sol.** Given :

(i) 
$$V(t) = 230\sqrt{2} \sin(\omega t)$$

(ii) 
$$i(t) = 10 \sin\left(\omega t - \frac{\pi}{3}\right) + 4 \sin\left(3\omega t - \frac{\pi}{6}\right) + 3 \sin\left(5\omega t - \frac{\pi}{3}\right)$$

(iii) f = 50 Hz

(iv) 
$$\omega = 2\pi \times 50 \text{ rad/sec}$$

Input power factor (IPF),

$$V(t)|_{RMS} = 230 \text{ V}, \ \dot{i}_1(t)|_{RMS} = \frac{10}{\sqrt{2}} \text{ A}$$

Fundamental displacement factor (FDF) =  $\cos \phi_1 = \cos \frac{\pi}{3} = \frac{1}{2}$ 

Where,  $\phi_1$  is the angle between voltage and fundamental component of current.

$$i(t)|_{RMS} = \sqrt{\left(\frac{10}{\sqrt{2}}\right)^2 + \left(\frac{4}{\sqrt{2}}\right)^2 + \left(\frac{3}{\sqrt{2}}\right)^2} = 7.905 \text{ A}$$

We know,  $IPF = Distortion factor \times Fundamental displacement factor$ 

$$IPF = g \times FDF$$

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Also, 
$$g = \frac{i_1(t)|_{RMS}}{i(t)|_{RMS}} = \frac{10/\sqrt{2}}{7.905} = 0.8946$$

Therefore, IPF  $= 0.8946 \times 0.5 = 0.4473$ 

Hence, the correct answer is 0.4473.

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#### **Question 34**

**Power System** 

Two balanced three-phase loads, as shown in the figure, are connected to a  $100\sqrt{3}$  V, three phase, 50 Hz main supply. Given :  $Z_1 = (18 + j24) \Omega$  and  $Z_2 = (6 + j8) \Omega$ . The ammeter reading, in amperes, is \_\_\_\_\_. (round off to nearest integer)  $100\sqrt{3}$  V γo Bo 20 (Range : 20 to 20) Ans. Sol. Given : Line to line voltage,  $V_{LL} = 100\sqrt{3}$  V (i) (ii)  $3-\phi$ , 50 Hz (iii)  $Z_1 = (18 + j24)\Omega$ (iv)  $Z_2 = (6+j8)\Omega$  $100\sqrt{3}$  V RO From above given figure, converting inner-star into delta. R **0-** $100\sqrt{3}$  V YO B O BO Per-phase equivalent impedance is,  $Z = Z_{nh} = Z_1 \parallel 3Z_2$  $Z_{ph} = \frac{3Z_1Z_2}{Z_1 + 3Z_2} = \frac{3(18 + j24)(6 + j8)}{18 + j24 + 3(6 + j8)}$ 

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$$Z_{ph} = \frac{3(18+j24)(6+j8)}{18+j24+18+j24}$$
$$Z_{ph} = 15\angle 53.10\Omega$$

In case of delta connection,

$$V_{ph} = V_{LL}$$
 and  $I_{LL} = \sqrt{3}I_{ph}$ 

Ammeter reading in ampere is,

$$I_{ph} = \frac{V_{ph}}{Z_{ph}} = \frac{100\sqrt{3}}{15\angle 53.10}$$
$$I_{ph} = 11.547\angle -53.10$$

Magnitude ammeter reading,

$$I_{LL} = \sqrt{3}I_{ph} = \sqrt{3} \times 11.547$$

 $I_{LL} = 20 \text{ A}$ 

Hence, the correct answer is 20.

#### **Question 35**

The frequencies of the stator and rotor currents flowing in a three-phase, 8-pole induction motor are 40 Hz and 1 Hz, respectively. The motor speed, in rpm, is \_\_\_\_\_\_. (round off to nearest integer)

ıce 20

#### Ans. 585 (Range : 580 to 590)

#### **Sol.** Given :

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- (i)  $3-\phi$  Induction motor
- (ii) Pole, P = 8
- (iii) Rotor current frequency,  $f_r = 1$ Hz
- (iv)Stator current frequency,  $f_s = 40$  Hz

Motor speed,  $N_r$  (in rpm)

Rotor current frequency,  $f_r = sf_s$ 

Slip, 
$$s = \frac{f_r}{f_s} = \frac{1}{40}$$

Synchronous speed,  $N_s = \frac{120 \times f_s}{P} = \frac{120 \times 40}{8} = 600$  rpm

Motor speed,  $N_r = (1-s)N_s = (1-0.025) \times 600 = 585$  rpm

Hence, the correct answer is 585 rpm.

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#### **Electrical Machine**

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## Q.36 to Q.65 Carry TWO Marks Each

#### **Question 36**

#### **Analog Electronics**

The output impedance of a non-ideal operational amplifier is denoted by  $Z_{out}$ . The variation in the magnitude of  $Z_{out}$  with increasing frequency, f, in the circuit shown below, is best represented by



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Sol. Given :  $G(s) = \frac{100}{s^2 + 0.1s + 100}$   $y(t) = a + b \sin(10t + \theta)$   $r(t) = 1 + 0.1 \sin 10t$   $r(t) = 1 + 0.1 \sin 10t \longrightarrow 100 \longrightarrow y(t) = a + b \sin(10t + \theta)$ Using super position theorem, Case 1 : r(t) = 1,  $\omega = 0$  rad/sec The steady state response,  $y_1(t) = \frac{100}{s^2 + 0.1s + 100} \times 1$   $y_1(t) = \frac{100}{(j\omega)^2 + 0.1j\omega + 100}$  $y_1(t) = \frac{100}{100} = 1$ 

$$y_1(t)\Big|_{\omega=0} = \frac{100}{100} = 1$$

**Case 2 :**  $r(t) = 0.1 \sin 10t$ ,  $\omega = 10$  rad/sec

The steady state response,

$$y_2(t) = \frac{100}{(j\omega)^2 + j0.1\omega + 100} \times 0.1\sin 10t$$

$$y_2(t) = \frac{10\sin 10t}{-100 + j + 100} = 10\sin\left(10t - 90^0\right)$$

Total steady state response,

$$y(t) = y_1(t) + y_2(t)$$
  
 $y(t) = 1 + 10\sin(10t - 90^{\circ})$ 

Given response,  $y(t) = a + b \sin(10t + \theta)$ 

$$a = 1$$
 and  $b = 10$ 

Hence, the correct option is (C).

#### **Question 38**

#### **Control System**

The open loop transfer function of a unity gain negative feedback system is given as  $G(s) = \frac{1}{s(s+1)}$ .

nce...(i)2004

...(ii)

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The Nyquist contour in the s-plane encloses the entire right half plane and a small neighborhood around the origin in the left half plane, as shown in figure below. The number of encirclements of the point (-1+j0) by the Nyquist plot of G(s), corresponding to the Nyquist contour, is denoted as N. Then N equals to



$$G(s) = \frac{1}{s(s+1)}$$

The Nyquist contour in the *s*-plane encloses the entire right half plane and a small neighborhood around the origin as shown in figure below



In the nyquist contour, the encirclement about origin is clockwise

[ACW]

N = P - Z

P = Number of right hand poles of open loop transfer function including the poles at origin

N = Number of anticlockwise encirclement about the critical point (-1+j0) in counter clockwise direction

Z = Number of right hand poles of closed loop transfer function

From the open loop transfer function

P=1 [Since G(s) has one pole at origin]

Characteristic equation,

1+G(s)=0

$$s^2 + s + 1 = 0$$

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Since, all the coefficient of characteristic equation of second order system are positive. System is stable i.e. no-poles in RHP.

$$Z = 0$$

 $N = P - Z \qquad [A.C.W.]$ 

$$N = 1 - 0$$

N = 1

Hence, the number of encirclement around the critical points (-1+j0) is 1.

Hence, the correct option is (D).

Method 2

Given open loop transfer function is,

$$G(s) = \frac{1}{s(s+1)}$$

The Nyquist contour in the *s*-plane encloses the entire right half plane and a small neighborhood around the origin as shown in figure below



Corresponding to the Nyquist contour the nyquist plot is shown below.



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**Note :** In nyquist plot ACW movement from  $\omega = 0^-$  to  $\omega = 0^+$ Since, in nyquist contour CW movement around the origin. Hence, the number of encirclement around the critical point (-1 + i0) in nyquist plot is 1. Hence, the correct option is (D). **E** Avoid this Mistake : Mistake 1 : Given open loop transfer function,  $G(s) = \frac{1}{s(s+1)}$ In general, the nyquist contour in the s-plane encloses the entire right half plane as shown in figure below Img(s) $\rightarrow \operatorname{Re}(s)$ For above nyquist contour, N = P - Z(Anticlockwise) Where, N = Number of encirclement about critical Point (-1+i0) in counter clockwise direction P = Number of right hand poles of open loop transfer function i.e. G(s)Z = Number of right hand poles of closed loop transfer function From the open loop transfer function P = 0Characteristic equation is given by, 1 + G(s) = 0 $s^2 + s + 1 = 0$ Since, all the coefficient of characteristic equation of second order system are positive. System is stable i.e. no poles in RHP. Z = 0N = P - ZN=0The number of encirclement about the point (-1+i0) in the Nyquist polt of G(s) is zero. Mistake 2 : Given open loop transfer function,  $G(s) = \frac{1}{s(s+1)}$ 

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Transfer function of above block diagrams is,

$$\frac{Y(s)}{R(s)} = \frac{\frac{100}{s(s+10)}}{1 + \frac{100}{s(s+10)}}$$
$$\frac{Y(s)}{R(s)} = \frac{100}{s^2 + 10s + 100}$$

Transfer function for standard second order system is given by

... (i)

$$\frac{C(s)}{R(s)} = \frac{\omega_n^2}{s^2 + 2\xi\omega_n s + \omega_n^2} \qquad \dots \text{ (ii)}$$

Where,  $\xi = Damping ratio$ ,  $\omega_n = Natural angular frequency$ .

On comparing equation (i) and equation (ii),

 $\omega_n^2 = 100; \ \omega_n = 10 \ rad/sec$ 

 $2\xi\omega_n = 10$ 

$$\xi = \frac{10}{2(10)} = \frac{1}{2} = 0.5$$

Hence, the correct option is (B).

#### **Question 40**

 $e^{A}$  denotes the exponential of a square matrix A. Suppose  $\lambda$  is an eigenvalue and v is the corresponding eigen-vector of matrix A.

Consider the following two statements :

```
Statement 1 : e^{\lambda} is an eigenvalue of e^{A}.
```

Statement 2 : v is an eigen-vector of  $e^{A}$ .

Which one of the following options is correct?

(A) Statement 1 is true and statement 2 is false.

(B) Statement 1 is false and statement 2 is true.

- (C) Both the statements are correct.
- (D) Both the statements are false.

#### Ans. C

**Sol.** Given : Exponential series,

$$e^{A} = 1 + \frac{A}{1!} + \frac{A^{2}}{2!} + \frac{A^{3}}{3!} + \dots \infty$$
$$e^{A} = 1 + \frac{A}{1!} + \frac{A^{2}}{2!} + \frac{A^{3}}{6!} + \dots \infty$$

Polynomial function of infinite series.

where,  $A_{n \times n} =$  Matrix,  $\lambda_A =$  Eigen value of A and V = Eigen vector corresponding to  $\lambda_A$ .

### **Mathematics**

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#### Method 1

Characteristics equation,

$$|A - \lambda I| = 0$$

$$\begin{bmatrix} 1 - \lambda & 0 & 0 \\ 0 & 4 - \lambda & -2 \\ 0 & 1 & 1 - \lambda \end{bmatrix} = 0$$

$$(1 - \lambda) [(4 - \lambda)(1 - \lambda) + 2] - 0 + 0 = 0$$

$$(1 - \lambda) [(4 - \lambda)(1 - \lambda) + 2] = 0$$

$$(1 - \lambda) [4 - 5\lambda + \lambda^{2} + 2] = 0$$

$$(1 - \lambda) [\lambda^{2} - 5\lambda + 6] = 0$$
[Characterized for the second second

Characteristics equation of matrix A]

Root of characteristic equation,

 $\lambda = 1, 2, 3$ [Eigen values of matrix A]  $(1-\lambda)(\lambda^{2}-5\lambda+6) = 0$   $\lambda^{2}-5\lambda+6-\lambda^{3}+5\lambda-6\lambda = 0$   $-\lambda^{3}+\lambda^{2}-6\lambda+6 = 0$   $\lambda^{3}-\lambda^{2}+6\lambda-6 = 0$ 

According to Cayley Hamilton's Theorem,  $A = \lambda$ 

$$A^3 - A^2 + 6A - 6I = 0$$

Multiplying  $A^{-1}$  both sides.

$$A^{-1}A^{3} - A^{-1}A^{2} + 6A^{-1}A - 6A^{-1} = 0$$
  

$$A^{2} - A + 6I = 6A^{-1}$$
  

$$6A^{-1} = A^{2} - A + 6I \qquad \dots (i)$$

As given in question,

$$6A^{-1} = A^2 + CA + DI$$
 C C C ...(ii)  
From equation (i) and (ii),

We get,

So,

C + D = -1 + 6 = 5

C = -1, D = 6

Hence, the correct option is (A).

#### Method 2

By Cayley Hamilton's Theorem,

Every square matrix satisfies its characteristics equation  $(A = \lambda)$ .

$$6A^{-1} = A^2 + CA + dI$$

...(i)

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GATE 2022 [Afternoon Session] **GATE AC** PAGE **Electrical Engineering** 42 Characteristics equation is given by,  $\lambda^3 - (tr)\lambda^2 + \sum (\text{Principle co-factor})\lambda - |A| = 0$ ...(ii) tr(A) = 1 + 4 + 1 = 61 0 0  $|A| = \begin{vmatrix} 0 & 4 & -2 \\ 0 & 1 & 1 \end{vmatrix} = 1(4+2) - 0 + 0 = 6$  $\sum$  (Principle cofactor) = 6+1+4=11 By equation (ii),  $\lambda^3 - 6\lambda^2 + 11\lambda - 6 = 0$  $A^{3}-6A^{2}+11A\lambda-6I=0$ Multiplying  $A^{-1}$  both sides.  $A^{-1}A^3 - A^{-1}A^2 + 6A^{-1}A - 6A^{-1} = 0$  $A^2 - A + 6I = 6A^{-1}$  $6A^{-1} = A^2 - A + 6I$ ...(iii) As given in question,  $6A^{-1} = A^2 + CA + DI$ ...(iv) From equation (iii) and (iv), We get, C = -1, D = 6So, C+D = -1+6=5Hence, the correct option is (A). **Power System Question 43** The fuel cost functions in rupees/hour for two 600 MW thermal power plants are given by Plant 1 :  $C_1 = 350 + 6P_1 + 0.004P_1^2$ Plant 2 :  $C_2 = 450 + aP_2 + 0.003P_2^2$ where  $P_1$  and  $P_2$  are power generated by plant 1 and plant 2, respectively, in MW and a is constant. The incremental cost of power ( $\lambda$ ) is 8 rupees per MWh. The two thermal power plants together meet a total power demand of 550 MW. The optimal generation of plant 1 and plant 2 in MW, respectively, are (A) 200, 350 (B) 350, 200 (C) 325, 225 (D) 250, 300 Ans. D Given : Fuel cost functions Sol. Plant 1 :  $C_1 = 350 + 6P_1 + 0.004P_1^2$  Rs/hr

Plant 2 :  $C_2 = 450 + aP_1 + 0.003P_2^2$  Rs/hr

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**Analog Electronics** 

For optimal generator, to share total load of 550 MW, incremental cost (I.C.) of units in operation must be same.

$$(IC)_1 = \frac{dC_1}{dP_1} = 6 + 0.008P_1 \text{ Rs/MWhr}$$
  
 $(IC)_2 = \frac{dC_2}{dP_2} = a + 0.006P_2 \text{ Rs/MWhr}$ 

For optimal generator,  $(IC)_1 = (IC)_2 = \lambda$ 

$$6+0.008P_1 = a+0.006P_2 = 8$$
 MW  
 $P_1 = \frac{8-6}{0.008} = 250$  MW  
 $P_2 = (550-250)$  MW = 300 MW  
 $P_1 = 250$  MW and  $P_2 = 300$  MW

Hence, the correct option is (D).

#### **Question 44**

The current gain  $(I_{out} / I_{in})$  in the circuit with an ideal current amplifier given below is





Here  $V_x$  is also a voltage across capacitor  $C_c$  so it can calculated as,



Compare equation (i) and (ii),

$$\frac{t}{C_f} I_{in} = \frac{t}{C_c} I_{out}$$
$$\frac{I_{out}}{I_{in}} = \frac{C_c}{C_f}$$

Hence, the correct option is (C).

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#### Method 2

Given circuit is shown below in the form of Laplace transform,



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From ampere's law,  $\overline{J} = \nabla \times \overline{H}$ Magnitude of current density,

$$|\overline{J}| = |\nabla \times \overline{H}|$$

$$\overline{J} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ H_x & H_y & H_z \end{vmatrix}$$

$$\overline{J} = \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ x^2 & x^2 y & x^2 y^2 z^2 \end{vmatrix}$$

$$\overline{J} = 2x^2 y z^2 \hat{i} - 2x y^2 z^2 \hat{j} + 2x y^2 \hat{k}$$
at point  $(x = 1, y = 2, z = 1)$  is,  

$$\overline{J} \Big|_{(1,2,1)} = 4\hat{i} - 8\hat{j} + 8\hat{k}$$

$$|\overline{J}| = 12 \text{ A/m}^2$$

*.*..

 $\vec{J}$ 

Hence, the correct option is (B).

#### **Question 46**

#### **Signals & Systems**

Let a causal LTI system be governed by the following differential equation  $y(t) + \frac{1}{4}\frac{dy}{dt} = 2x(t)$ , where

x(t) and y(t) are the input and output respectively. Its impulse response is

(B)  $8e^{-\frac{1}{4}t}u(t)$ (A)  $8e^{-4t}u(t)$ (C)  $2e^{-4t}u(t)$ (D)  $2e^{-\frac{1}{4}t}u(t)$ 

Ans.

Given differential equation is,  $y(t) + \frac{1}{4} \frac{dy}{dt} = 2x(t)$ Sol.

Taking Laplace transform on both sides, we get

$$Y(s) + \frac{1}{4}sY(s) = 2X(s)$$
$$\left(\frac{s}{4} + 1\right)Y(s) = 2X(s)$$
$$\frac{Y(s)}{X(s)} = \frac{2}{\frac{s}{4} + 1}$$

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 $\frac{Y(s)}{X(s)} = \frac{8}{s+4}$  which is the transfer function of this system.

:. Impulse response will be, 
$$h(t) = L^{-1} \left[ \frac{8}{s+4} \right] = 8e^{-4t}u(t)$$

Hence, the correct option is (A).

#### **Question 47**

#### **Signals & Systems**

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Let an input  $x(t) = 2\sin(10\pi t) + 5\cos(15\pi t) + 7\sin(42\pi t) + 4\cos(45\pi t)$  is passed through an LTI system having an impulse response,

$$h(t) = 2\left(\frac{\sin(10\pi t)}{\pi t}\right)\cos(40\pi t)$$

The output of the system is

(A)	$2\sin(10\pi t) + 5\cos(15\pi t)$	(B)	$2\sin(10\pi t) + 4\cos(45\pi t)$

(C) 
$$7\sin(42\pi t) + 4\cos(45\pi t)$$
 (D)  $5\cos(15\pi t) + 7\sin(42\pi t)$ 

С Ans.

Sol. Given impulse response is,

$$h(t) = 2\left(\frac{\sin 10\pi t}{\pi t}\right)\cos(40\pi t)$$

$$h(t) = \frac{\sin 50\pi t - \sin 30\pi t}{\pi t}$$

$$h(t) = \frac{\sin 50\pi t}{\pi t} - \frac{\sin 30\pi t}{\pi t}$$

$$h(t) = h_1(t) - h_2(t)$$
Where,  $h_1(t) = \frac{\sin 50\pi t}{\pi t}$  and  $h_2(t) = \frac{\sin 30\pi t}{\pi t}$ 
The Fourier transform of  $h(t)$  is,
$$h(t) \leftarrow FT \rightarrow H(\omega) = H_1(\omega) - H_2(\omega)$$

$$H(\omega) = H_1(\omega) - H_2(\omega)$$

$$H_1(\omega) = H_1(\omega) - H_2(\omega)$$

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Multiplying both sides by a scalar quantity 'a' $ay_1(t) = ax_1(e^t)$ ...(i) For input  $x_2(e^t)$ , output will  $y_2(t)$  $y_{2}(t) = x_{2}(e^{t})$ Multiplying both sides by a scalar quantity b' $b y_2(t) = b x_2(e^t)$ ...(ii) Adding equation (i) and (ii) we get  $a y_1(t) + b y_2(t) = a x_1(e^t) + b x_2(e^t)$ ...(iii) Let for input  $a x_1(e^t) + b x_2(e^t)$ , output is  $y_3(t)$  $y_{2}(t) = a x_{1}(e^{t}) + b x_{2}(e^{t})$ But  $a x_1(e^t) + b x_2(e^t) = a y_1(t) + b y_2(t)$  $y_3(t) = a y_1(t) + b y_2(t)$ ÷. Hence, system satisfies both additivity and homogeneity law. ... The system is a linear system. From the given system  $y(t) = x(e^t)$  $y(0) = x(e^0) = x(1)$  $y(1) = x(e^1) = x(e) = x(2.71)$ So, present value of output depends on future value of input.  $\therefore$  The given system is non causal. Hence, the correct option is (B). **Question 49** Signals & Systems The discrete time Fourier series representation of a signal x[n] with period N is written as  $x[n] = \sum_{k=0}^{N-1} a_k e^{j(2kn\pi/N)}$ . A discrete time periodic signal with period N=3, has the non-zero Fourier series

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coefficients :  $a_{-3} = 2$  and  $a_4 = 1$ . The signal is

(A) 
$$2+2e^{-\left(j\frac{2\pi}{6}n\right)}\cos\left(\frac{2\pi}{6}n\right)$$
 (B)  $2+2e^{\left(j\frac{2\pi}{6}n\right)}\cos\left(\frac{2\pi}{6}n\right)$   
(C)  $1+2e^{\left(j\frac{2\pi}{6}n\right)}\cos\left(\frac{2\pi}{6}n\right)$  (D)  $1+2e^{\left(j\frac{2\pi}{3}n\right)}\cos\left(\frac{2\pi}{6}n\right)$ 

Ans. C

GATE 2022 [Afternoon Session] GATE AC*l* PAGE **Electrical Engineering** 50 steps to success. **Given**:  $x[n] = \sum_{k=0}^{N-1} a_k e^{j\left(\frac{2\pi kn}{N}\right)}$ Sol. Also given that N=3,  $a_{-3}=2$  and  $a_4=1$ As the Fourier series coefficients are periodic in nature, so  $a_{N+k} = a_k$ (*N* is period of the signal)  $a_{N-k} = a_{-k}$ For k = 3,  $a_{N-3} = a_{-3}$  $a_{3-3} = a_{-3}$  $a_0 = a_{-3} = 2$ For k = 4,  $a_{N+1} = a_1$  $a_{3+1} = a_1$ (:: N=3) $a_{4} = a_{1} = 1$ Thus,  $a_0 = 2, a_1 = 1$ . On expanding x(n), we get  $x[n] = a_0 + a_1 e^{\frac{j2\pi n}{3}}$  $x[n] = 2 + e^{\frac{j2\pi n}{3}}$  $x[n] = 1 + 1 + e^{\frac{j2\pi n}{3}}$  $x[n] = 1 + e^{\frac{j\pi n}{3}} \left[ e^{-j\frac{\pi}{3}n} + e^{j\frac{\pi}{3}n} \right]$ e 2  $x[n] = 1 + e^{\frac{j\pi n}{3}} \cdot 2\cos\frac{\pi n}{2}$  $x[n] = 1 + 2e^{\frac{j\pi n}{3}} \cdot \cos \frac{2\pi n}{6}$ Hence, the correct option is (C). **W** Key Point For a periodic signal x[n] has period N, the discrete time Fourier series coefficient  $a_k$  is also periodic in nature  $a_{k+N} = a_k$  and  $a_{-k+N} = a_{-k}$ .

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Let,  $f(x, y, z) = 4x^2 + 7xy + 3xz^2$ . The direction in which the function f(x, y, z) increases most rapidly at point P = (1, 0, 2) is

(A) 
$$20\hat{i} + 12\hat{k}$$
 (B)  $20\hat{i} + 7\hat{j} + 12k$ 

(C)  $20\hat{i} + 7\hat{j}$  (D)  $20\hat{i}$ 

#### Ans. B

**Sol.** Given, scalar point function,

$$f(x, y, z) = 4x^2 + 7xy + 3xz^2$$

Gradient gives the direction in which the directional derivative will be maximum.

Grad 
$$(f) = \nabla \cdot f$$
  

$$\nabla \cdot f = \left(\hat{i} \frac{\partial}{\partial x} + \hat{j} \frac{\partial}{\partial y} + \hat{k} \frac{\partial}{\partial z}\right) (4x^2 + 7xy + 3xz^2)$$

$$\nabla \cdot f = (8x + 7y + 3z^2)\hat{i} + (7x)\hat{j} + (6xz)\hat{k}$$

At point P(1, 0, 2),

$$\nabla \cdot f = (8 \times 1 + 7 \times 0 + 3 \times 2^2)\hat{i} + (7 \times 1)\hat{j} + (6 \times 1 \times 2)\hat{k}$$
$$\nabla \cdot f = 20\hat{i} + 7\hat{j} + 12\hat{k}$$

Hence, the correct option is (B).

#### **Question 51**

Let R be a region in the first quadrant of the xy plane enclosed by a closed curve C considered in counterclockwise direction. Which of the following expressions does not represent the area of the region R?



#### **Mathematics**

## **Mathematics**

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Green's theorem, 
$$\oint_C \phi dx + \psi dy = \iint_S \left( \frac{\partial \psi}{\partial x} - \frac{\partial \phi}{\partial y} \right) dx \, dy$$

Checking from options,

From option (A) :

$$\oint_C x dy = \iint_S (1-0) dx dy = \iint_S dx dy \qquad [\phi = 0, \psi = x]$$

[Area of region *R* in anticlockwise direction]

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**Mathematics** 

$$\frac{1}{2} \oint_C x dy - y dy = \frac{1}{2} \iint_S (1 - (-1)) dx dy \quad [\phi = -y, \psi = x]$$
$$= \frac{1}{2} \iint_S 2 dx dy = \iint_S dx dy$$
[Area of region *R* in anticlockwise direction]

From option (C) :

$$\oint_C dxdy = \text{Area of } \frac{\text{region } R}{\text{region } R}$$

From option (D) :

$$\oint_C y dx = \iint_S (0 - (1)) dx dy$$
$$= \iint_C -1 dx dy = -\iint_S dx dy$$

 $\left[\phi = y, \psi = 0\right]$ 

[Area of region *R* in clockwise direction]

Hence, the correct option is (D).

#### **Question 52**

Ans.

Sol.

Let  $\vec{E}(x, y, z) = 2x^2\hat{i} + 5y\hat{j} + 3z\hat{k}$ . The value of  $\iint_V (\vec{\nabla} \cdot \vec{E}) dV$ , where *V* is the volume enclosed by the unit cube defined by  $0 \le x \le 1, 0 \le y \le 1$ , and  $0 \le z \le 1$ , is (A) 3 (B) 8 (C) 10 (D) 5 (D) 5 (D) 5 (C) (D) 5 (C)

 $\nabla \cdot \vec{E} = 4x + 8$ 

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question)

$$\iiint_{V} (\vec{\nabla} \cdot \vec{E}) \, dV = \int_{x=0}^{1} \int_{y=0}^{1} \int_{z=0}^{1} (4x+8) \cdot dx \, dy \, dz \qquad (\because \quad dV = dx \, dy \, dz \text{ according to}$$
$$\iiint_{V} (\vec{\nabla} \cdot \vec{E}) \, dV = 4 \frac{x^{2}}{2} \Big|_{0}^{1} y \Big|_{0}^{1} z \Big|_{0}^{1} + 8x \Big|_{0}^{1} y \Big|_{0}^{1} z \Big|_{0}^{1}$$
$$\iiint_{V} (\vec{\nabla} \cdot \vec{E}) \, dV = 4 \left(\frac{1}{2}\right) (1) (1) + 8(1) (1) (1) = 10$$

Hence, the correct option is (C).

#### **Question 53**

#### **Electromagnetic Field**

As shown in the figure below, two concentric conducting spherical shells, centered at r=0 and having radii r=c and r=d are maintained at potentials such that the potential V(r) at r=c is  $V_1$  and V(r) at r=d is  $V_2$ . Assume that V(r) depends only on r, where r is the radial distance. The expression for V(r) in the region between r=c and r=d is





There is no charge present in side conducting spherical shell ( $\rho_v = 0$ ), so according to Laplace equation  $\nabla^2 V(r) = 0$ Laplacian formula, (only consider *r*-direction component)  $\nabla^2 V = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial V(r)}{\partial r} \right) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial V(r)}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \left( \frac{\partial^2 V(r)}{\partial \theta^2} \right)$  $\frac{1}{r^2}\frac{\partial}{\partial r}\left(r^2\frac{\partial V(r)}{\partial r}\right) = 0$  $\frac{\partial}{\partial r} \left( r^2 \frac{\partial V(r)}{\partial r} \right) = 0$ Integrate the above equation on both side with respect to r,  $r^2 \frac{\partial V(r)}{\partial r} = k_1$ ( $\therefore k_1$  is arbitrary constant)  $\frac{\partial V(r)}{\partial r} = \frac{k_1}{r_2}$ Again integrate above equation on both side with respect to r,  $\int \partial V(r) = \int \frac{k_1}{r^2} \partial r$  $V(r) = -\frac{k_1}{r} + k_2$ ... (i) (::  $k_2$  is arbitrary constant) Given at r = c;  $V(r = c) = V_1$  $V_1 = \frac{-k_1}{c} + k_2$ ...(ii) Given at r = d;  $V(r = d) = V_2$  $\frac{-k_1}{d} + k_2 = V_2$ ..(iii) From equation (ii) and (iii),  $\frac{-k_1}{d} + \frac{k_1}{c} = V_2 - V_1$  Since 2  $k_1 = \frac{(V_2 - V_1)}{d - \frac{c}{cd}}$  $k_1 = \frac{(V_2 - V_1)cd}{d - c}$ Put the value of  $k_1$  in equation (ii),  $k_2 = V_1 + \frac{k_1}{2}$ 

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$$k_{2} = V_{1} + \frac{(V_{2} - V_{1})cd}{(d - c)c}$$
$$k_{2} = \frac{-V_{1}c + V_{2}d}{V_{2}}$$

$$z_2 = \frac{1}{d-c}$$

Put the value of  $k_1$  and  $k_2$  in equation (i),

So, 
$$V(r) = \frac{cd(V_1 - V_2)}{(d - c)r} + \frac{(V_2 d - V_1 c)}{d - c}$$

Hence, the correct option is (B).

#### **Question 54**

Let the probability density function of a random variable x be given as  $f(x) = ae^{-2|x|}$ . The value of 'a' is

### Ans. 1 (Range : 0.99 to 1.01)

**Sol.** Given :  $f(x) = ae^{-2|x|}, x \in (-\infty, \infty)$ 

Probability Density Function (P.D.F.) for a valid PDF. Area under the complete curve is unity.

$$\int_{-\infty}^{\infty} f(x) dx = 1$$

$$\int_{-\infty}^{\infty} a e^{-2|x|} dx = 1$$

$$\left[ \because |x| = \begin{cases} +x \ ; \ x \ge 0 \\ -x \ ; \ x < 0 \end{cases} \right]$$

$$2 \int_{0}^{\infty} a e^{-2x} dx = 1$$

$$2a \int_{0}^{\infty} e^{-2x} dx = 1$$

$$2a \left[ \frac{e^{-2x}}{-2} \right]_{0}^{\infty} = 1$$

$$2a \left[ \frac{e^{-2x}}{-2} \right]_{0}^{\infty} = 1$$

$$2a \left[ e^{-\infty} - e^{0} \right] = 1$$

$$-a(0-1) = 1$$

$$a = 1$$

Hence, the correct answer is 1.

#### **Question 55**

**Network Theory** 

In the circuit shown below, the magnitude of the voltage  $V_1$  in volts, across the 8 k $\Omega$  resistor is \_\_\_\_\_ (round off to nearest integer)

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Substituting the value of *I* from equation (ii) in equation (i),

$$-75 + 0.5V_{1} + 2000 \left[ \frac{V_{1}}{8000} \right] = 0$$
$$-75 + 0.5V_{1} + 0.25V_{1} = 0$$
$$0.75V_{1} = 75$$
$$V_{1} = 100 \text{ V}$$

Hence, the value of voltage across  $8k\Omega$  resistance is 100 V.

#### **Question 56**

#### **Electrical Machine**

Two generating units rated for 250 MW and 400 MW have governor speed regulations of 6% and 6.4%, respectively, from no load to full load. Both the generating units are operating in parallel to share a load of 500 MW. Assuming free governor action, the load shared in MW, by the 250 MW generating unit is \_\_\_\_\_. (round off to nearest integer)

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\_\_\_\_\_\_ (100 mm of 100 mm to minutest mitiger)

# Ans. 200 (Range : 188 to 192 or 198 to 202)

**Sol.** Given :

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(i) Generating unit 1 :  $P_{1r} = 250 \text{ MW}$ 

Speed regulations =6%

## Generating unit 2 :

 $P_{2r} = 400 \text{ MW}$ 

Speed regulation = 6.4%

(ii) Load = 500 MW

 $P_1 + P_2 = 500 \text{ MW} \dots (i)$ 

Load shared by 250 MW generating unit  $(P_1)$ .

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#### **Question 57**

**Power System** 

A 20 MVA, 11.2 kV, 4-pole, 50 Hz alternator has an inertia constant of 15 MJ/MVA. If the input and output powers of the alternator are 15 MW and 10 MW, respectively, the angular acceleration in mechanical degree/ $s^2$  is \_\_\_\_\_. (round off to nearest integer)

#### Ans. 75 (Range : 74 to 76)

#### **Sol.** Given :

- (i) S = 20 MVA
- (ii) Voltage (V) = 11.2 kV
- (iii) Number of poles, P = 4
- (iv) Inertia constant, H = 15 MJ/MVA
- (v) Input power,  $P_{in} = 15 \text{ MW} = P_m$
- (vi) Output power,  $P_e = 10 \text{ MW}$

Angular acceleration \_\_\_\_\_ mech.degree/ $s^2$ 

Swing equation,  $M \frac{d^2 \delta}{dt^2} = P_m - P_e$ 

$$\alpha = \frac{d^2 \delta}{dt^2} = \frac{P_m - P_e}{M} \text{ elect.degree/} s^2 \qquad \dots(i)$$

Note :

We know, 
$$\theta_e = \frac{P}{2} \theta_m$$
  
 $\frac{d\theta_e}{dt} = \frac{P}{2} \frac{d\theta_m}{dt}$   
 $\omega_e = \frac{P}{2} \omega_m$   
 $\alpha_e = \frac{P}{2} \alpha_m$   
 $\alpha_m = \frac{2}{P} \alpha_e$   
**ince2004**

Angular acceleration in mech.deg./ $s^2 = \frac{2}{P} \times$  angular acceleration in elect.deg./ $s^2$ .

So equation (i),

$$\frac{d^2\delta}{dt^2} = \frac{P_m - P_e}{M} \text{ elect.deg./ } s^2$$
$$\frac{d^2\delta}{dt^2} = \frac{P_m - P_e}{M} \times \frac{2}{P} \text{ mech.deg./ } s^2$$

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$$\frac{d^2\delta}{dt^2} = \frac{P_m - P_e}{\frac{GH}{\pi f}} \times \frac{2}{P} \text{ mech.deg./ } s^2$$
$$\frac{d^2\delta}{dt^2} = \frac{(15 - 10) \times 180 \times 50}{20 \times 15} \times \frac{2}{4} \text{ mech.deg/} s^2$$
$$\frac{d^2\delta}{dt^2} = 75 \text{ mech.deg/} s^2$$

Hence, the correct answer is 75.

#### **Question 58**

Consider an ideal full-bridge single-phase DC-AC inverter with a DC bus voltage magnitude of 1000 V. The inverter output voltage v(t) shown below, is obtained when diagonal switches of the inverter are switched with 50% duty cycle. The inverter feeds a load with a sinusoidal current given by,

 $i(t) = 10\sin\left(\omega t - \frac{\pi}{3}\right) A$ , where  $\omega = \frac{2\pi}{T}$ . The active power, in watts, delivered to the load is \_\_\_\_\_. (round off to nearest integer)

$$0 \qquad 0.5T \qquad T \qquad f \sec$$

#### Ans. 3183 (Range : 3170 to 3190)

**Sol.** Given :

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(i) DC bus voltage magnitude 
$$V_{dc} = 1000 \text{ V}$$

(ii) 
$$i(t) = 10\sin\left(\omega_0 t - \frac{\pi}{3}\right)$$
, where  $\omega = \frac{2\pi}{T}$ 

The Fourier series expansion of the given voltage v(t) is,

 $v(t) \blacktriangle$ 

$$v(t) = \sum_{n=1,3,5}^{\infty} \frac{4V_{dc}}{n\pi} \sin(n\omega_0 t) \qquad (\because v(t) \text{ has half wave symmetry})$$

$$\therefore v(t)\big|_{n=1} = \frac{4 \times 1000}{\pi} \sin(\omega_0 t)$$

The active power delivered to load in watts,

Power, 
$$P = v(t)\Big|_{n=1}$$
 (rms)× $i(t)\Big|$  (rms)× $\cos\phi = \frac{4 \times 1000}{\pi \times \sqrt{2}} \times \frac{10}{\sqrt{2}} \times \left(\cos\frac{\pi}{3}\right) = 3183$  W

Hence, the correct answer is 3183.

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#### **Power Electronics**

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#### **Question 59**

#### **Power Electronics**

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For the ideal AC-DC rectifier circuit shown in the figure below, the load current magnitude is  $I_{dc} = 15$  A and is ripple free. The thyristors are fired with a delay angle of  $45^{\circ}$ . The amplitude of the fundamental

component of the source current, in amperes, is \_\_\_\_\_. (round off to two decimal places)



#### Ans. 17.65 (Range : 17.30 to 18)

#### **Sol.** Given :

Single phase symmetrical semi-converter

- (i) Load current magnitude,  $I_{DC} = 15$  A
- (ii) Firing angle,  $\alpha = 45^{\circ}$

A symmetrical single phase semi converter is shown below,



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$$(I_{SI})_{peak} = \frac{4I_{DC}}{\pi} \cos\left(\frac{\alpha}{2}\right) = \frac{4 \times 15}{\pi} \times \cos\left(\frac{45}{2}\right) = 17.64 \text{ A}$$
  
Hence, the correct answer is 17.65

Hence, the correct answer is 17.65.

#### **Power Electronics**

#### **Question 60**

A 3-phase grid-connected voltage source converter with DC link voltage of 1000 V is switched using sinusoidal Pulse Width Modulation (PWM) technique. If the grid phase current is 10 A and the 3-phase complex power supplied by the converter is given by (-4000 - j3000) VA, then the modulation index used in sinusoidal PWM is \_\_\_\_\_. (round off to two decimal places)

#### Ans. 0.471 (Range : 0.46 to 0.48)

**Sol.** Given :

- (i) 3-phase grid connected voltage source converter with DC link.
  - $V_{dc} = 1000$  V using sinusoidal pulse with modulation (PWM)



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Form figure are can see that,

(ii) 
$$I_{L(mmx)} = 16 \text{ A}$$
  
(iii)  $I_{L(mmx)} = 12 \text{ A}$   
(v)  $T_{ON} = DT = 20 \text{ }\mu\text{s}$   
(v)  $T = T_{ON} + T_{OFF} = 20 + 30 = 50 \text{ }\mu\text{s}$   
Now,  $D = \text{Duty ratio} = \frac{T_{OX}}{T} = \frac{20}{50} = \frac{2}{5}$   
We know,  $I_{L(ngy)} = \frac{I_{L(mxx)} + I_{L(min)}}{2} = \frac{12 + 16}{2} = 14 \text{ A}$   
Also  $I_{L(ngy)} = \frac{I_0}{1 - D} = \frac{I_0}{1 - \frac{2}{5}}$   
 $\therefore I_0 = 14 \times \frac{2}{5} = 8.4 \text{ A}$   
For buck boost converter,  
The ripple in capacitor voltage = The ripple in output voltage  
 $\Delta V_0 = \Delta V_c = 1V$   
As  $\Delta V_c = \frac{DI_0}{fC} = \frac{\frac{2}{5} \times \frac{14 \times 3}{5}}{\frac{1}{50 \times 10^{-6} \times C}}$   
 $\therefore I = \frac{\frac{2}{5} \times \frac{14 \times 3}{5} \times 50 \times 10^{-6}}{C}$   
 $C = 168 \,\mu\text{F}$   
Hence, the correct answer is 168  $\mu\text{F}$ .

A 280 V, separately excited DC motor with armature resistance of 1  $\Omega$  and constant field excitation drives a load. The load torque is proportional to the speed. The motor draws a current of 30 A when running at a speed of 1000 rpm. Neglect frictional losses in the motor. The speed, in rpm, at which the motor will run, if an additional resistance of value 10  $\Omega$  is connected in series with the armature, is \_\_\_\_\_. (round off to nearest integer)

## Ans. 483 (Range : 480 to 485)

## **Sol.** Given :

- (i) Separately excited DC motor
- (ii) Terminal voltage,  $V_t = 280$  V

(iii)Armature resistance,  $R_a = 1 \Omega$ 

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(iv)Constant field excitation i.e.  $\phi$  = Constant

(v) Load torque is proportional to speed i.e  $T \propto N$ 

(vi)  $I_{a1} = 30$  A at  $N_1 = 1000$  rpm

(vii) Additional resistance  $R_{ext} = 10 \Omega$ 

Motor speed in rpm  $(N_2)$  when additional resistance is connected in series with armature.

Back emf,  $E_b = K\phi\omega$ 

 $E_b \propto N$  (::  $\phi$  = Constant)

Where,  $\omega$  is angular speed in rad/sec and N is speed in rpm.

Load Torque,

$$T = K \phi I_a$$

$$T \propto I_a$$
 (:: $\phi$  = Constant)

Where,  $I_a$  is armature current.

Also 
$$T \propto N$$
 (Given)

$$N \propto I_a$$

Now back EMF at 1000 rpm when  $I_{a1} = 30$  A is,

$$E_{b1} = V_t - I_{a1}R_a = 280 - 30 \times 1$$
  
 $E_{b1} = 250 \text{ V}$ 

Armature current when external resistance is added in series

$$\therefore N \propto I$$

$$\frac{N_1}{N_2} = \frac{I_{a1}}{I_{a2}} \qquad \textbf{A} \qquad \textbf{T} \qquad \textbf{E}$$

$$I_{a2} = \frac{N_2}{N_1} \times I_{a1} = \frac{30}{1000} N_2 \qquad \textbf{ince 2004}$$

$$I_{a2} = 0.03 N_2 \qquad \dots (i)$$

Back emf after adding external armature resistance is,

$$E_{b2} = V_t - I_{a2}(R_a + R_{ext})$$

From equation (i),

$$E_{b2} = 280 - 0.03N_2(1+10)$$
$$E_{b2} = 280 - 0.33N_2$$

Now as  $E_b \propto N$ 

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... (ii)

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So,  $\frac{E_{b2}}{E_{b1}} = \frac{N_2}{N_1}$ 

$$\frac{280 - 0.33N_2}{250} = \frac{N_2}{1000}$$
$$N_2 = 4 \times (280 - 0.33N_2)$$
$$N_2 = 482.75 \text{ rpm}$$

Hence, the correct answer is 482.75 rpm.

## **Question 63**

#### **Electrical Machine**

A 4-pole induction motor with inertia of 0.1 kg-  $m^2$  drives a constant load torque of 2 Nm. The speed of the motor is increased linearly from 1000 rpm to 1500 rpm in 4 seconds as shown in the figure below. Neglect losses in the motor. The energy, in joules, consumed by the motor during the speed change is



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Energy delivered to load =T (Area under the curve)

Energy delivered to load = 
$$T \times \left\{ \left( 4 \times 1000 \times \frac{2\pi}{60} \right) + \left( \frac{1}{2} \times 4 \times (1500 - 1000) \times \frac{2\pi}{60} \right) \right\} = 1047.2$$
 Joules

Total energy consumed by motor = 685.4 + 1047.2 = 1732.5 Joules

Hence, the correct answer is 1732.5.

#### **Question 64**

#### **Electrical Machine**

A star-connected 3-phase, 400 V, 50 kVA, 50 Hz synchronous motor has a synchronous reactance of 1 ohm per phase with negligible armature resistance. The shaft load on the motor is 10 kW while the power factor is 0.8 leading. The loss in the motor is 2 kW. The magnitude of the per phase excitation emf of the motor, in volts, is \_\_\_\_\_ (round off to nearest integer).

#### Ans. 244.5 (Range : 240 to 248)

#### **Sol.** Given :

- (i)  $3-\phi$ , star connected synchronous motor.
- (ii) Terminal voltage,  $V_L = 400$  V
- (iii)Rated KVA S = 50 KVA
- (iv)Frequency, f = 50 Hz
- (v) Synchronous reactance,  $X_s = \frac{1 \Omega}{ph}$

(vi)Negligible armature resistance

(vii) Shaft load,  $P_{sh} = 10 \text{ kW}$ 

(viii) Load power factor,  $\cos \phi = 0.8$  leading

(ix)Losses = 2 kW

Magnitude of the per phase excitation of the motor (in volts),



As armature resistance is negligible of synchronous motor,

So, 
$$P_d = P_{input}$$
 and  $P_{input} = \sqrt{3}V_L I_L \cos \phi$   
 $\sqrt{3}V_L I_L \cos \phi = 12 \text{ kW}$   
 $I_L = \frac{12000}{\sqrt{3} \times 400 \times 0.8} = 21.65 \text{ A}$   
 $I_L = I_L = 21.65 \text{ A}$ 

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Now for synchronous motor in case of leading power factor.

$$E_{ph}^{2} = (V_{ph} \cos \phi - I_{a}R_{a})^{2} + (V_{ph} \sin \phi + I_{a}X_{a})^{2}$$
$$E_{ph}^{2} = \left(\frac{400}{\sqrt{3}} \times 0.8 - 0\right)^{2} + \left(\frac{400}{\sqrt{3}} \times 0.6 + 21.65 \times 1\right)^{2}$$
$$E_{ph} = 244.54 \text{ V}$$

Hence, the correct answer is 244.5 V.

#### **Question 65**

#### **Electrical Machine**

... (ii)

steps to success.

A 3-phase, 415 V, 4-pole, 50 Hz induction motor draws 5 times the rated current at rated voltage at starting. It is required to bring down the starting current from the supply to 2 times of the rated current using a 3-phase autotransformer. If the magnetizing impedance of the induction motor and no load current of the autotransformer is neglected, then the transformation ratio of the autotransformer is given by \_\_\_\_\_. (round off to two decimal places)

#### Ans. 0.63 (Range : 0.61 to 0.65)

#### **Sol.** Given :

- (i) 3-φ, 415 V, 4-pole, 50 Hz Induction motor.
- (ii) At Rated Voltage, at Starting (DOL),  $I_{st} = I_{sc} = 5I_{fl}$  ... (i)
- (iii) By using auto-transformer  $I_{st} = x^2 I_{sc} = 2I_{fl}$

Where *x* is transformation ratio.

Transformation ration 'x' of auto transformer

From equation (i) and (ii),

$$x^2(I_{sc}) = 2I_f$$

$$x^2(5I_{fl}) = 2I_{fl}$$

$$x^2 = \frac{2}{5}$$
  
 $x = \sqrt{\frac{2}{5}} = 0.632$  Since 2004

Hence the correct answer is 0.632.

\*\*\*\*

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